

UNIVERSITY OF SASKATCHEWAN
ELECTRICAL ENGINEERING
EE313.3 ELECTRICAL MACHINES I
FINAL EXAMINATION

Instructor: N. Chowdhury

Time: 3 hours

December 1997

Notes: (a) This is a closed book examination.

(b) Formula sheets are attached.

(c) Record in your answer book(a) all necessary steps and calculations.

Marks

- 15 ☒ The open-circuit characteristic data of a dc shunt generator taken at 1400 r.p.m. are shown below:

Field current (A)	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0
Term. voltage (V)	92	165	237	303	349	382	415	438	456	469

☒ Draw the open-circuit characteristic curve of the dc generator at 1400 r.p.m.

☒ Determine the no-load terminal voltage of the dc generator at 1200 r.p.m. if the field circuit resistance is adjusted to 220 ohms.

☒ Determine the generated voltage, terminal voltage and power output of the generator at 1200 r.p.m. when it delivers 120 A to a load. The shunt field resistance is 220 ohms and the armature circuit resistance is 0.2 ohm. Neglect armature reaction.

- 16 ☒ A wye-connected, three-phase, 60-Hz, 4-pole alternator has 48 slots and 26 conductors per slot. The machine is lap-wound with double-layer. The coils span 11 slots. The alternator has a fundamental flux per pole of 0.06 Wb, a 3rd harmonic flux per pole of 0.005 Wb and a 5th harmonic flux per pole of 0.002 Wb. Determine the following:

☒ the pitch factor(s) of the winding, $K_p = 0.9914$ $K_{p1} = 0.9577$
☒ the distribution factor(s) of the winding, $K_{p3} = -0.7239$ $K_{d3} = 0.6633$
☒ emf per coil, $K_{p5} = 0.7934$ $K_{d5} = 0.2053$
☒ the open-circuit phase voltage, and
☒ the open-circuit line-to-line voltage.

- 8 ☒ A three-phase ac synchronous generator is connected to a three-phase system at an infinite bus. With the help of a phasor diagram, explain what would happen if the prime-mover input of the synchronous generator is increased from its previous level while the excitation, the frequency and the terminal voltage are held at their previous levels.

- 15 ☒ A three-phase, wye-connected, 480-V, 30-Hp, 60-Hz, four-pole induction motor has the following equivalent circuit constants in ohms per phase referred to the stator:

EE 313.3 Electrical Mac
Final Examination
December 1997

Marks

$$R_1 = 0.2,$$



Exam File Provided By
The UoF IEEE Student Branch

ieee.usask.ca

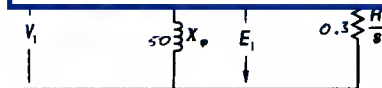


Figure 1. Equivalent circuit of an induction motor.

The motor is connected directly to a three-phase, 60-Hz, 480-V source. Determine the line current and the internal torque during starting.

☒ A three-phase, 11000-V, 60-Hz, wye-connected, cylindrical-rotor synchronous generator is delivering 2000 kVA at 0.82 lagging power factor when connected to a three-phase, 11000-V, 60-Hz infinite bus. The machine has a resistance of 1.5 Ω and a synchronous reactance of 14 Ω per phase.

- 10 ☒ (a) Determine the excitation voltage, the power angle and real and reactive power output of the generator. Draw a phasor diagram showing all voltages and the armature current.

- 15 ☒ The excitation of the generator is increased by 10 percent while the prime-mover power is held at its previous level. Determine the stator current, the power angle and the reactive power supplied by the generator. [Hint: Do not neglect the stator resistance.]

- 21 6. Mark the following statements as TRUE or FALSE. If you mark a statement as FALSE, briefly mention your reason(s) for doing so.

- ☒ The net effect of armature reaction in a dc machine can be considered as a reduction in the armature current.
☒ In a dc machine, pole face windings are used to neutralize the reactance voltage.
☒ In dc machines, interpoles are used to improve commutation.
☒ The speed of a dc shunt motor varies linearly as a function of its field flux.
☒ Short-pitched coils are used in three-phase alternators to improve the waveform of the voltage.
☒ Synchronous generators connected to infinite buses usually operate at lagging power factors.
☒ A synchronous motor connected to an infinite bus can be operated at a leading power factor.
☒ Synchronous motors are self-starting and, therefore, can be started with a load.

- ☒ The flux produced by the stator of an induction motor rotates at synchronous speed.
- ☒ The rotor of an induction motor rotates at synchronous speed.
- ☒ The frequency of the voltage induced in the rotor of an induction motor would be 60 Hz, if the machine were supplied from a balanced, three-phase, 60 Hz source.
- ☒ In an induction motor, the maximum internal torque occurs when the rotor current is at its maximum.
- ☒ The magnitude of the maximum internal torque in an induction motor can be increased by increasing the rotor resistance, provided all other parameters remain constant.
- ☒ The no-load test of an induction motor is ordinarily taken at a frequency lower than the rated frequency with rated voltage applied to the stator.

THE END

DC MACHINES

EMF, and Electromotive Force: $e = \vec{v} \times \vec{B} l$, $f = \vec{i} \times \vec{B} l$, v = velocity, i = current, B = field, l = length, e = EMF, f = force

Lenz's Law: $e = -\frac{\delta \lambda}{\delta t} = -\frac{\delta(N\phi)}{\delta t}$, λ = flux linkage passed through, N = #turns, ϕ = flux

Avg. Generated EMF: $e_g = \frac{P\phi n Z}{60a}$, e_g = generated emf, ϕ = flux per pole, P = # poles, Z = # conductors, a = parallel paths, n = (RPM).

$$\theta_{ad} = \frac{P}{2} \theta_{mech}$$

	Generators	DC Motor: Shunt	DC Motor: Series
Terminal Voltage	$V_t = E_g - I_a R_a$		
Back EMF		$E_g = V_t - I_a R_a$	$E_g = V_t - I_a R_a - I_f R_f$
Back EMF/Speed	$E_g = K_a \phi_a \omega_m$	$E_g = K_a \phi_a \omega_m$	$E_g = K_a \phi_a \omega_m$
Electromagnetic Power		$P_e = E_g I_a$	$P_e = E_g I_a$
Input Power		$V_t I_t = V_t I_a + V_t I_f$	$V_t I_t = E_g I_a + I_a^2 R_a + I_a^2 R_f$
Output Power	$P_{out} = V_t I_{a-rated}$	$P_{out} = P_e - \text{mech losses}$	$P_{out} = P_e - \text{mech losses}$
Torque/Power		$T_e \omega_m = P_e = E_g I_a$	$T_e \omega_m = P_e = E_g I_a$
Torque/Current		$T_e = K_a \phi_a I_a$	$T_e = K_a \phi_a I_a$
Neglecting Saturation and armature reaction		$\phi_a = K_f I_f$ $E_g = K_a I_a \omega_m$ $T_e = K_a I_a I_f$	$\phi_a = K_f I_f$ $E_g = K_a I_a \omega_m$ $T_e = K_a I_a^2$

V_t = terminal voltage, E_g = generated emf, I_a = Armature current, I_f = field current, I_L = Load/Line current, R_a = armature resistance plus effective brush-commutator contact resistance, R_f = field resistance, ω_m = angular speed (radians) = $2\pi n/60$ where n = speed (RPM), P_e = Electromagnetic Power

Speed Regulation: $SR = \frac{N_{NL} - N_{FL}}{N_{FL}}$, N = speed

Voltage Regulation: $VR = \frac{V_{NL} - V_{rated}}{V_{rated}}$, V_t = terminal voltage

SYNCHRONOUS GENERATORS (Round Rotor)

Voltage per coil: $E_{coil} \text{ (rms)} = (2\pi/\sqrt{2}) f_a N \phi_n = 4.44 f_a N \phi_n$, f = frequency, N = #turns/coil, ϕ = flux/pole, subscript n = harmonic

Distribution factor: $K_d = \frac{\sin(0.5nm\alpha)}{m \sin(0.5n\alpha)}$, n = harmonic, m = # individual coils, α = slot angle, angle between adjacent slots (θ_{ad})

Pitch factor: $K_p = \sin\left(\frac{nP}{2}\right)$, P = pitch, n = harmonic

Voltage Generated: $E_{gen} \text{ (rms)} = 4.44 K_w n f_a \phi_n N_t$, K_w = winding factor (K_p, K_d), N_t = #turns/phase = (mN) where m = #coils, N = #turns/coil, ϕ_n = flux/pole, subscript n = harmonic

